

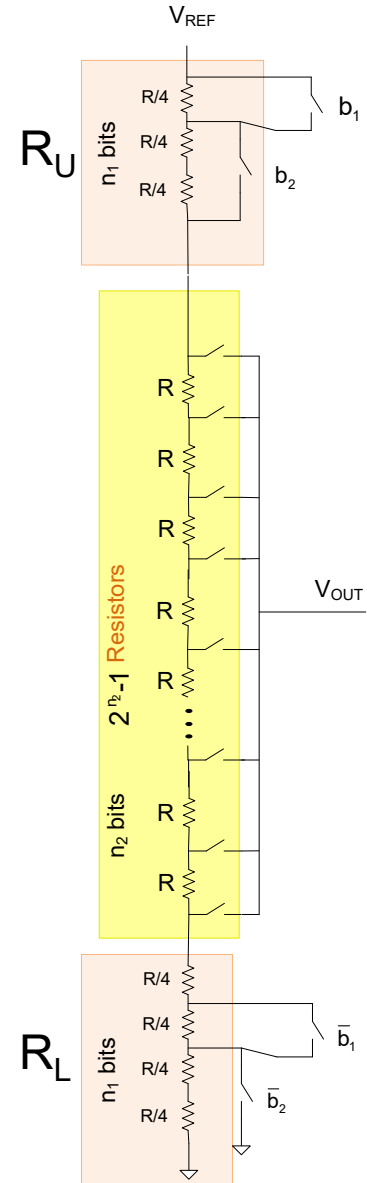
# EE 435

## Lecture 34

Switches

Current Steering DACs

# Basic R-String DAC



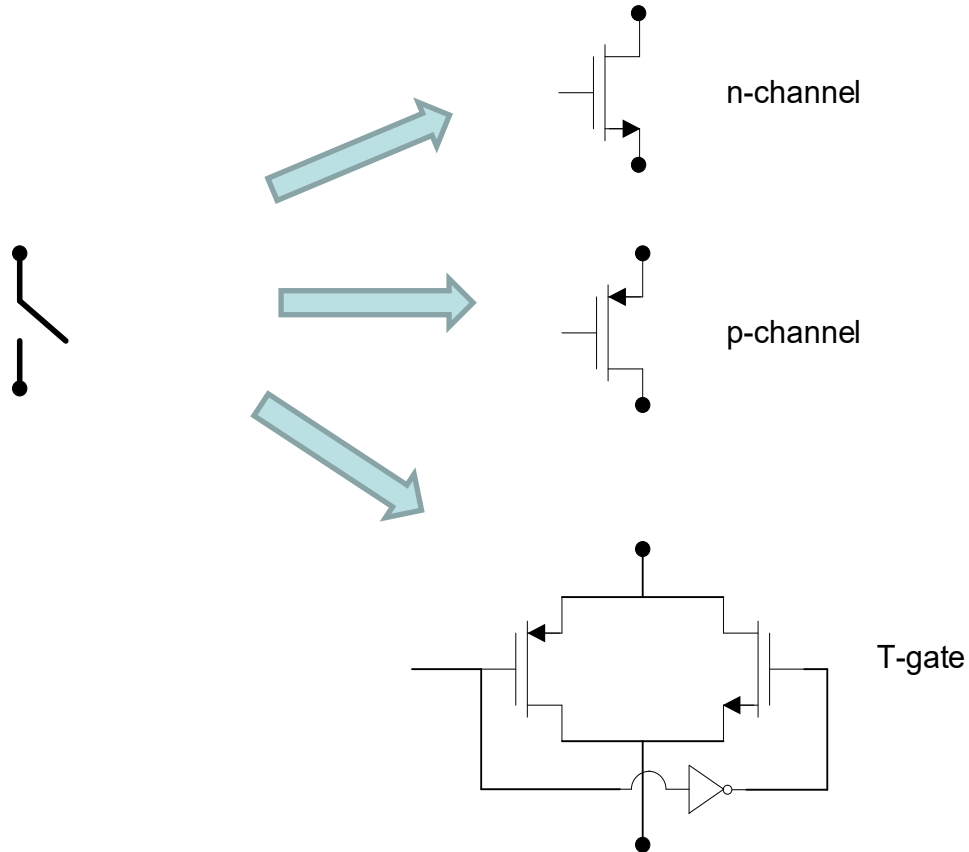
For all  $b_1$  and  $b_2$ ,  $R_U + R_L = R$

- Another Segmented DAC structure
- Can be viewed as a “dither” DAC
- Often  $n_1$  is much smaller than  $n_2$
- Dither can be used in other applications as well

# Switches used extensively in data converters !

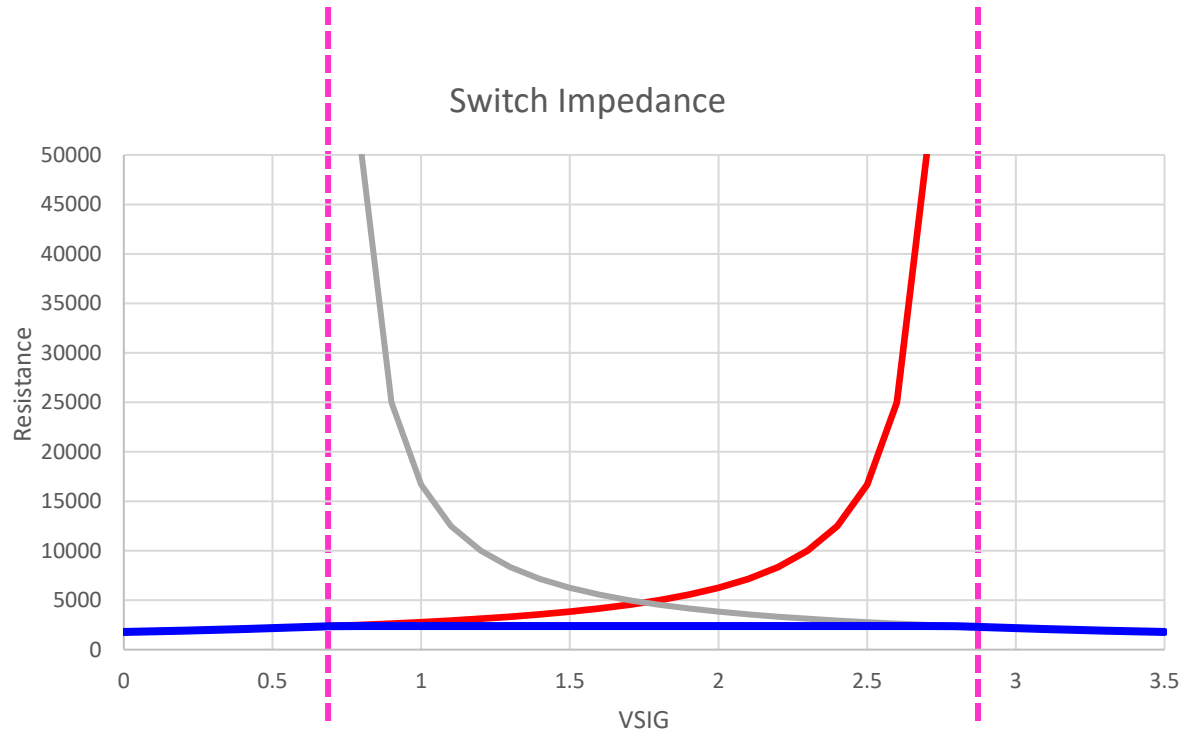
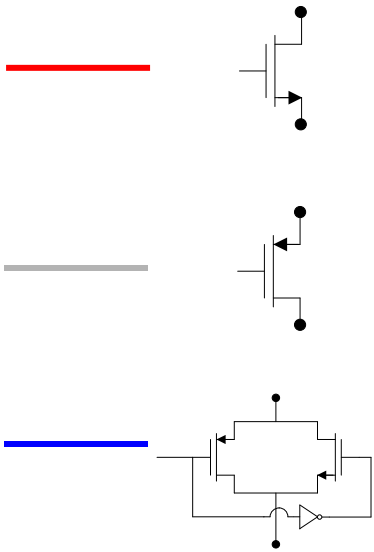
## Switch Implementation Issues

### Basic Simple Switches



# Switch Implementation Issues

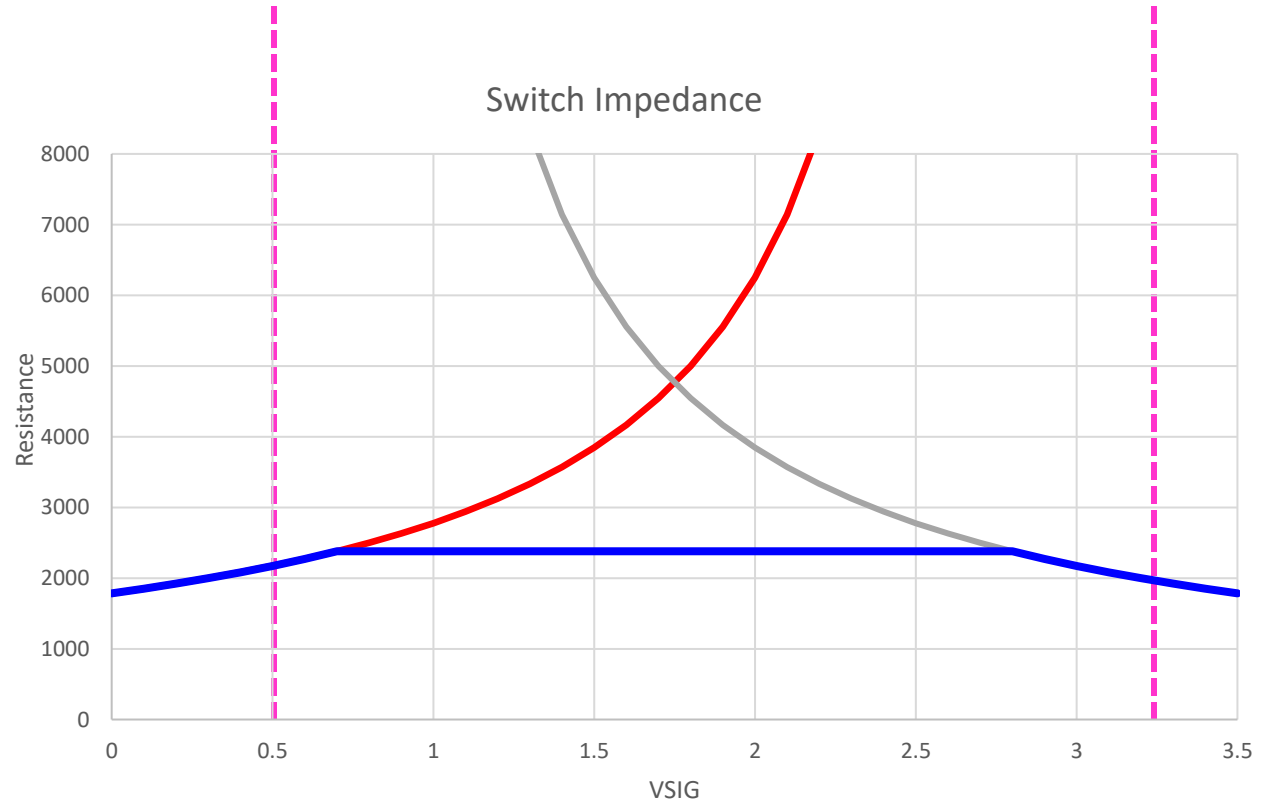
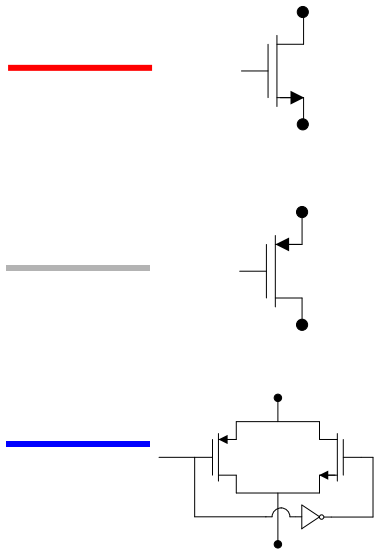
$V_{THn}=0.7$   
 $V_{THp}=-0.7$   
 $W_p=3W_n$   
 $L_p=L_n$   
 $V_{DD}=3.5V$



$V_{SIG}$ : Voltage on switch when ON

# Switch Implementation Issues

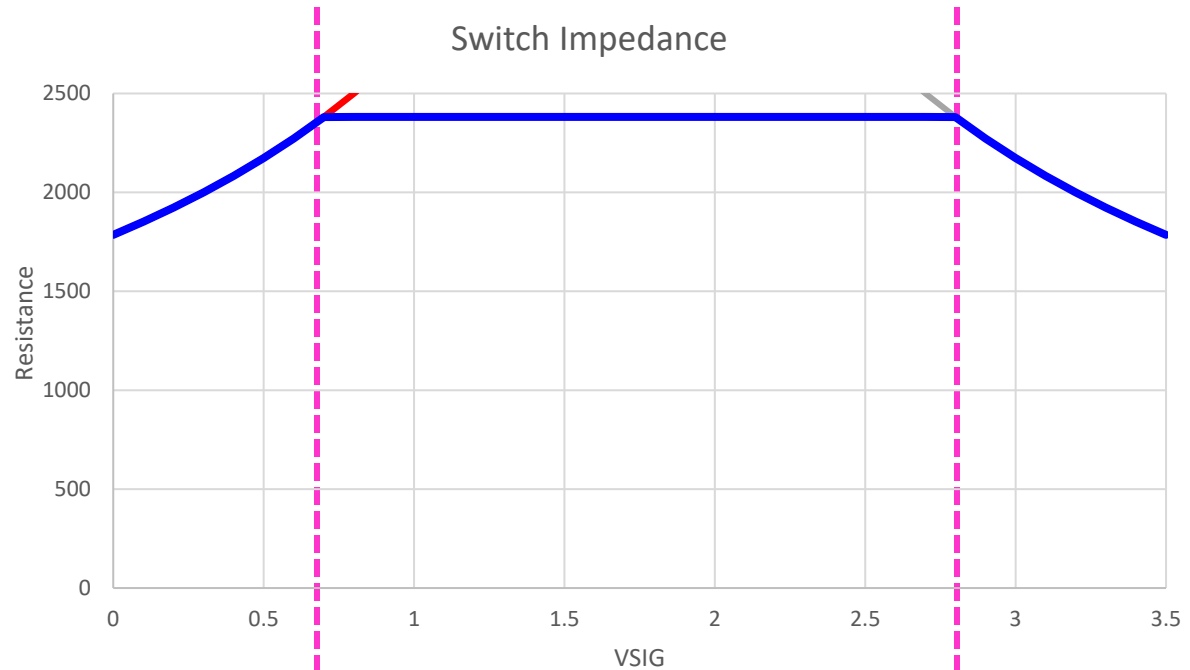
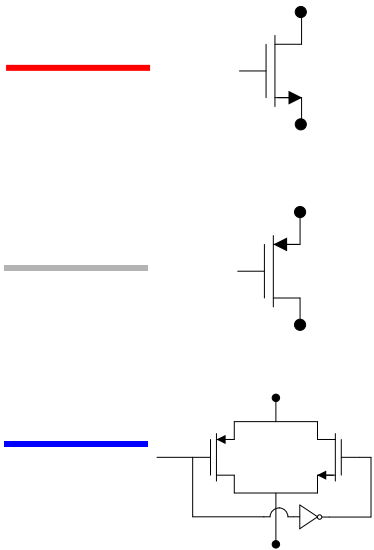
$V_{THn} = 0.7$   
 $V_{THp} = -0.7$   
 $W_p = 3W_n$   
 $L_p = L_n$   
 $V_{DD} = 3.5V$



$V_{SIG}$ : Voltage on switch when ON

# Switch Implementation Issues

$V_{THn}=0.7$   
 $V_{THp}=-0.7$   
 $W_p=3W_n$   
 $L_p=L_n$   
 $V_{DD}=3.5V$

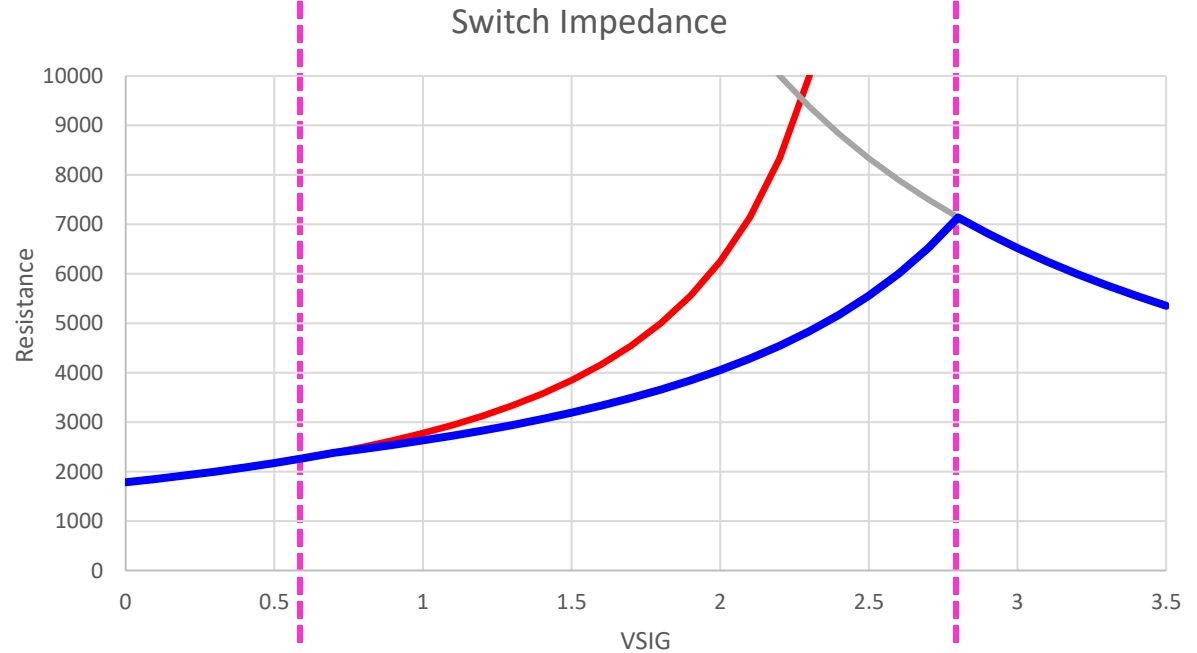
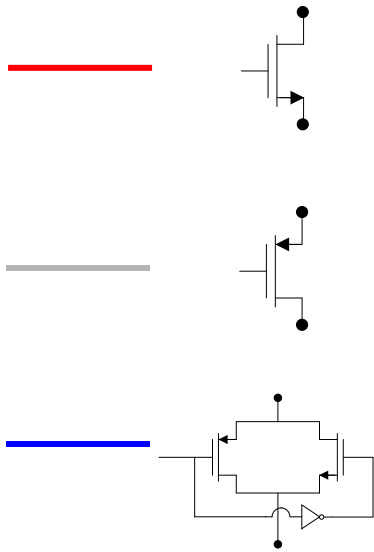


Transmission Gate Impedance Can be Reasonably constant

# Switch Implementation Issues

## Equal-Sized Switches

$V_{THn}=0.7$   
 $V_{THp}=-0.7$   
 $W_p=W_n$   
 $L_p=L_n$   
 $V_{DD}=3.5V$



# Switch Implementation Issues

Equal-Sized Switches  
High Threshold Voltages

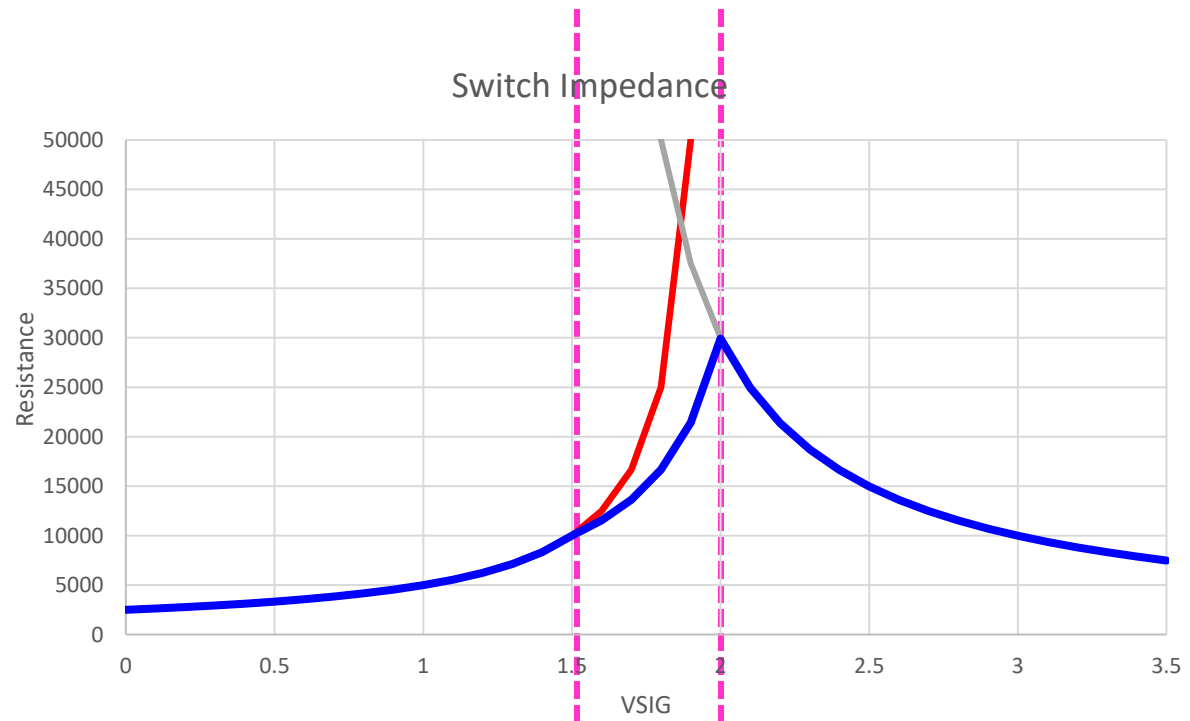
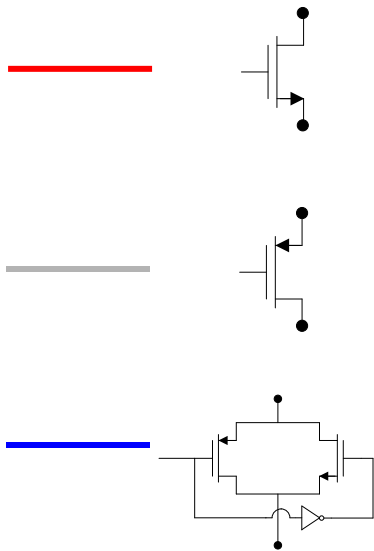
$$V_{THn} = 1.50$$

$$V_{THp} = -1.5$$

$$W_p = W_n$$

$$L_p = L_n$$

$$V_{DD} = 3.5V$$



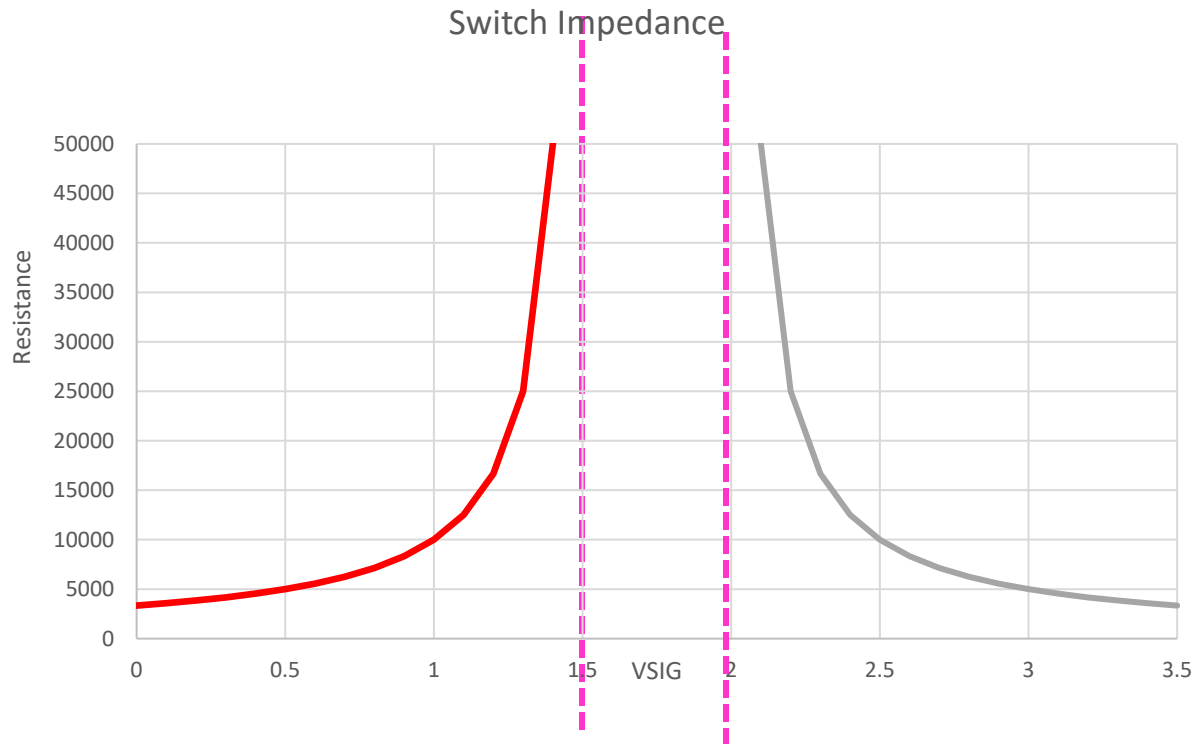
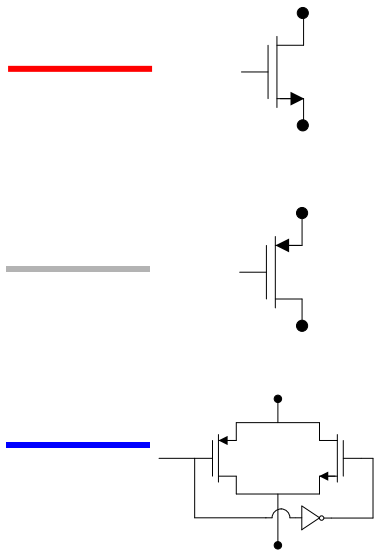
Even Transmission Gate Does Not Perform Well



# Switch Implementation Issues

$$\begin{aligned}V_{THn} &= 2.0 \\ V_{THp} &= -2.0 \\ W_p &= 3W_n \\ L_p &= L_n \\ V_{DD} &= 3.5V\end{aligned}$$

Tough unlikely, this is what would happen if very high threshold devices were used



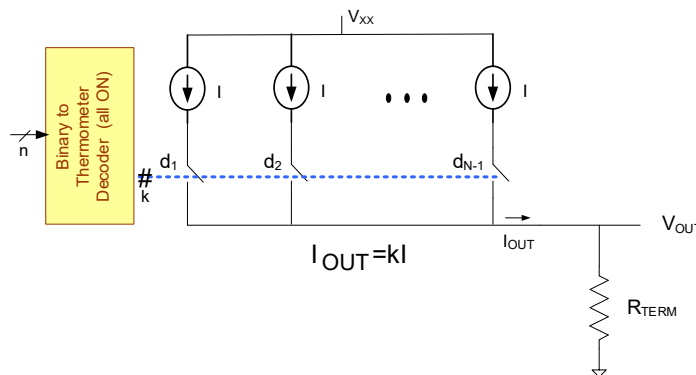
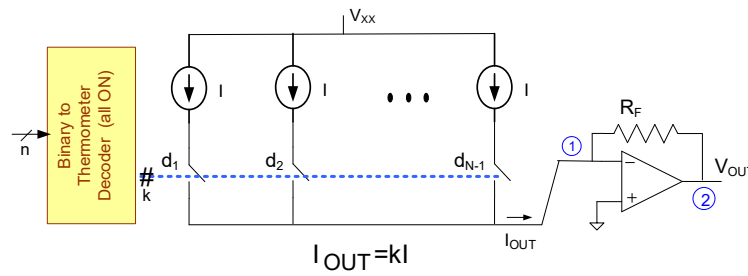
Gap where neither switch is working

# Current Steering DACs

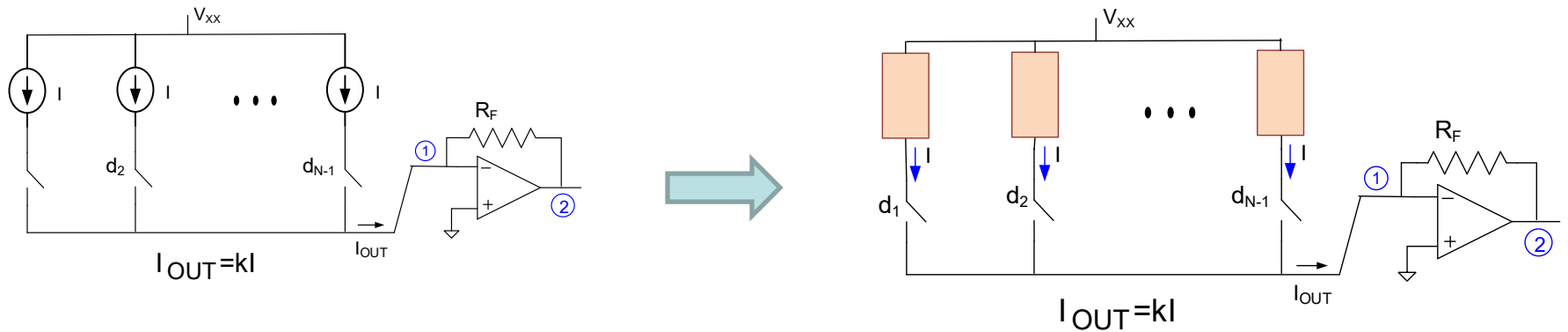
Current will be “steered” to a resistive load (on chip)

Output could be a current (user supplies load)

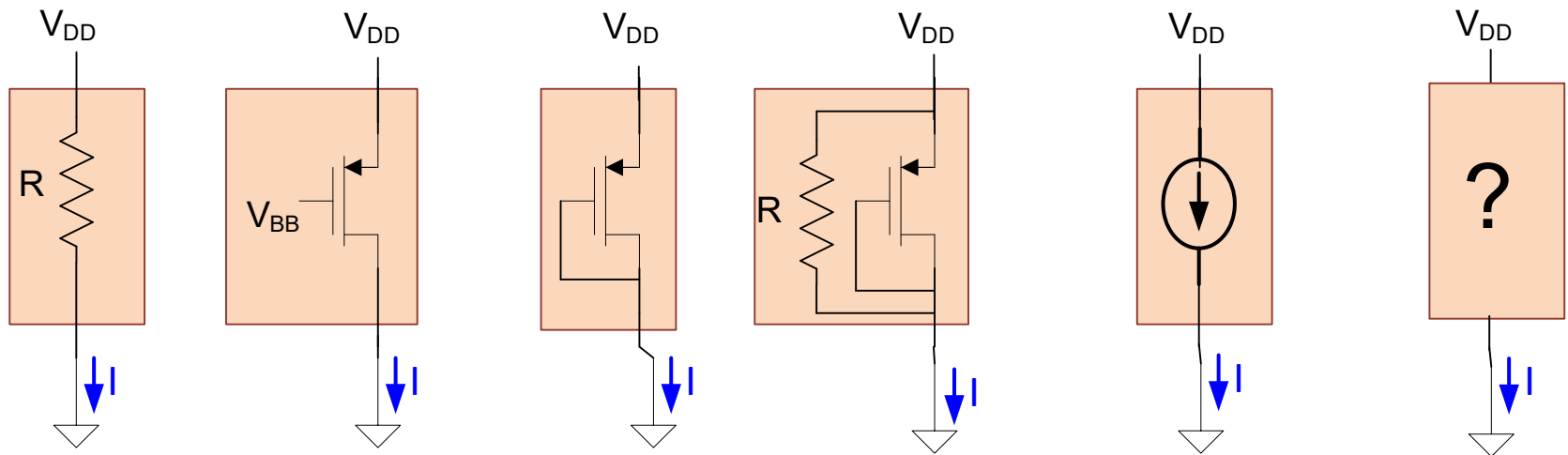
## Basic Concept of Current Steering DACs



# Current Steering DACs

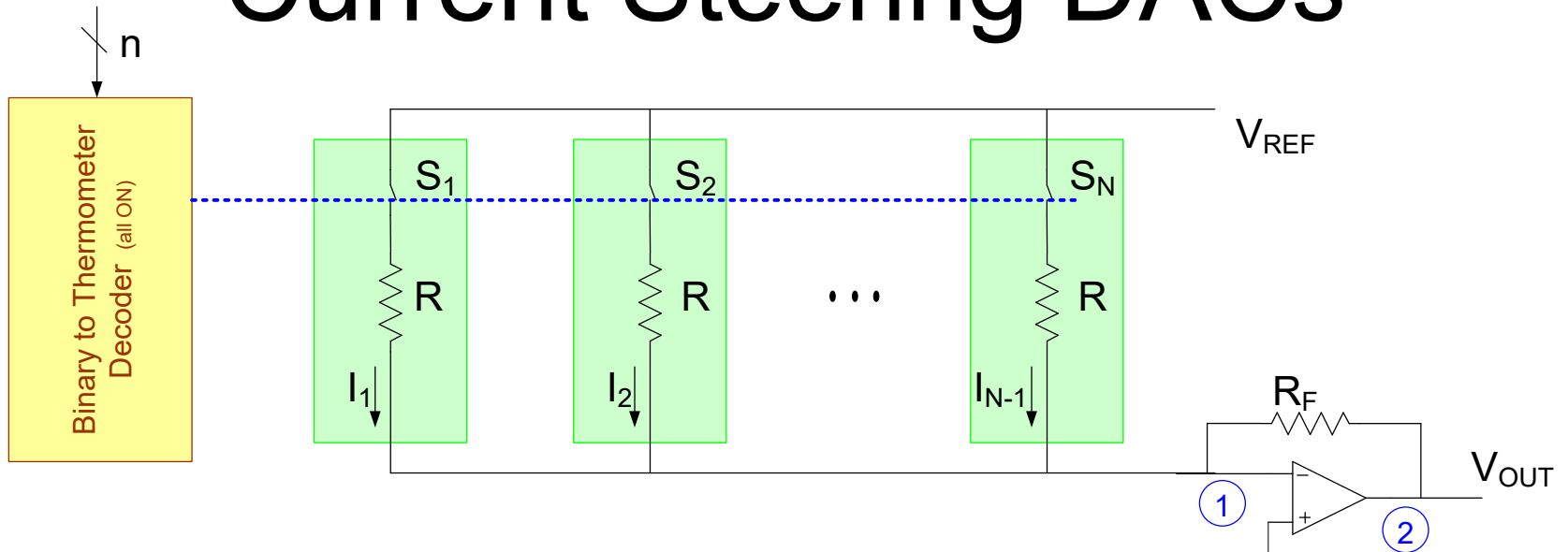


What is important is the current generated, not whether it comes from a “current source”



Many potential current generator blocks, just require that all be ideally identical

# Current Steering DACs

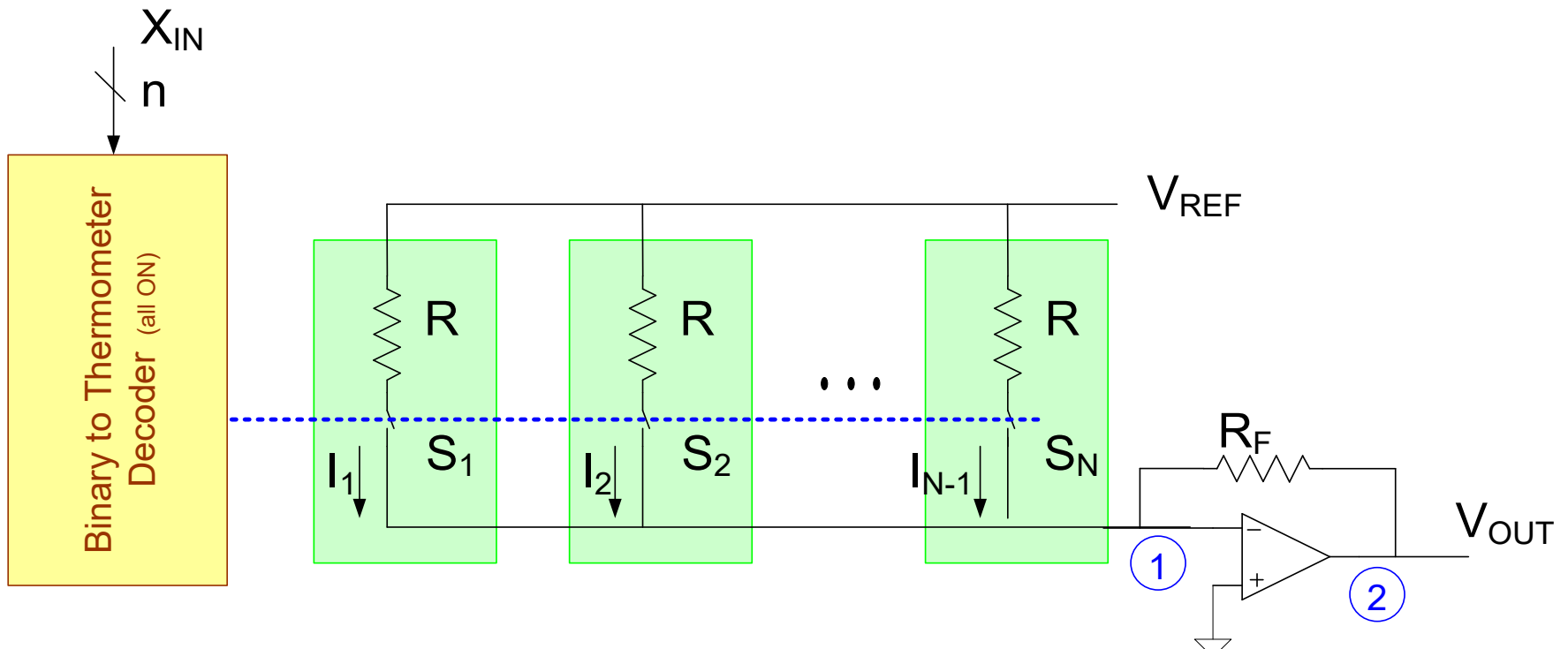


## Inherently Insensitive to Nonlinearities in Switches and Resistors

- Termed “top plate switching”
- Thermometer coding
- Excellent DNL properties
- INL may be poor, typically near mid range
- INL is a random variable with variance approximately proportional to area
- Area gets large for good yield with large  $n$
- Each additional bit of resolution requires a factor of 2 increase in area if same sized resistors are used
- Each additional bit of resolution requires another factor of 4 increase in area to maintain the same yield

$$\sigma = \frac{A_{PEL}}{\sqrt{A}}$$

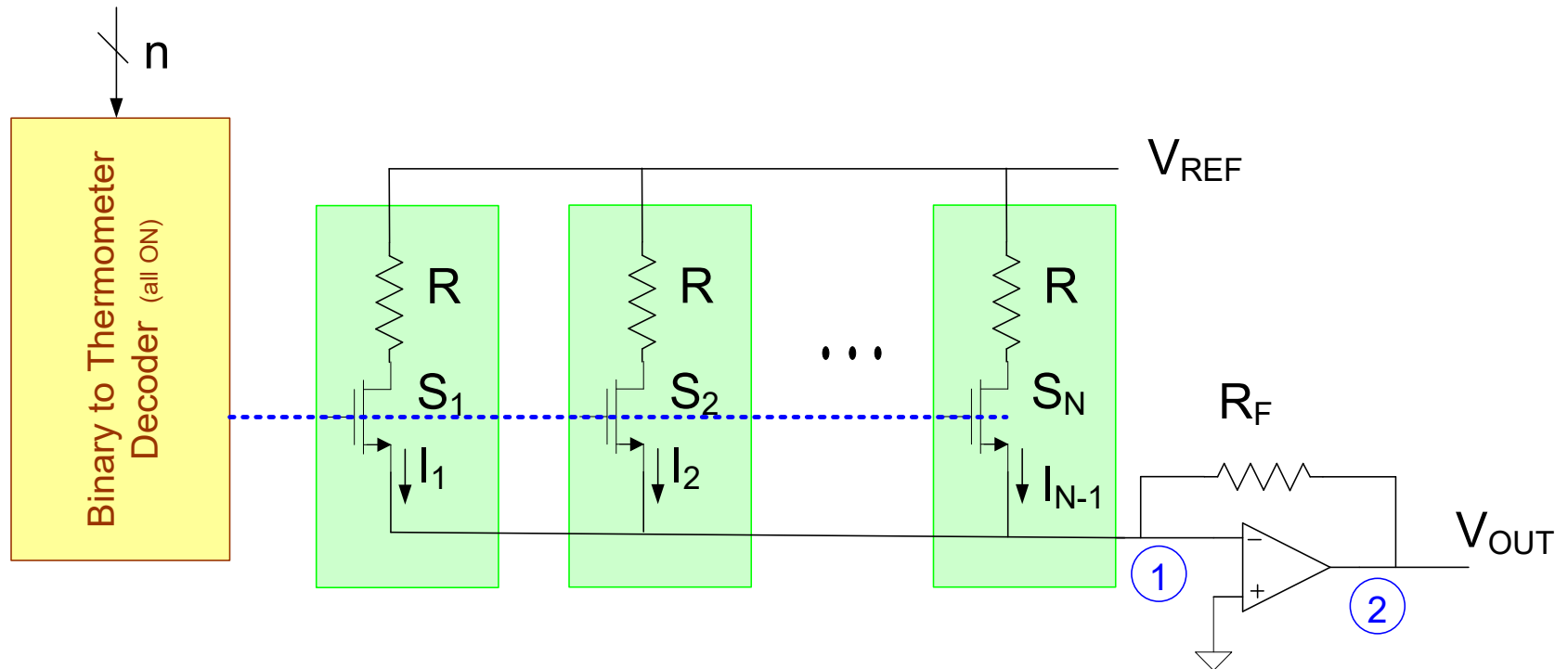
# Current Steering DACs



**Inherently Insensitive to Nonlinearities in Switches and Resistors**  
**Smaller ON resistance and less phase-shift from clock edges**

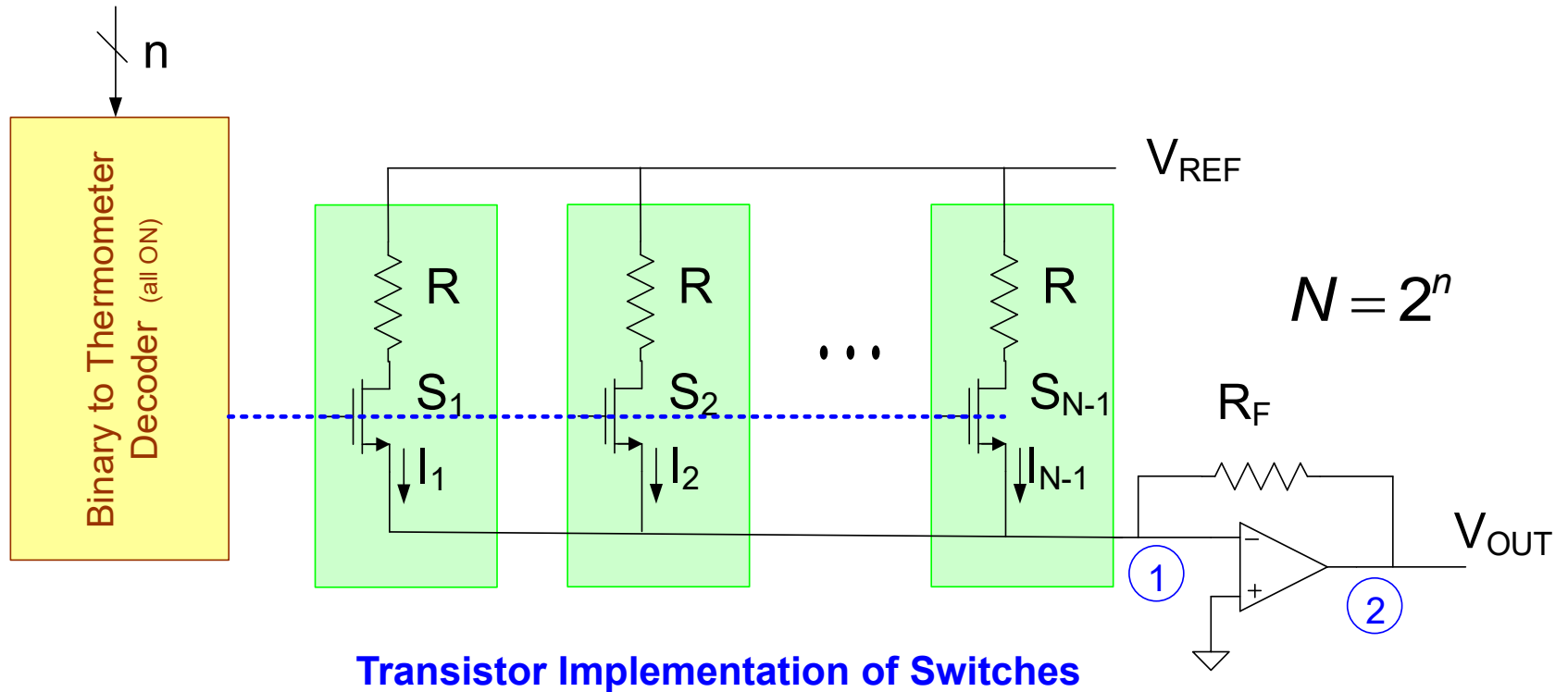
- Termed “bottom plate switching”
- Thermometer coded

# Current Steering DACs



**Transistor Implementation of Switches**

# Current Steering DACs



How should the op amp be compensated?

Assume k switches are on  $0 < k < N-1$

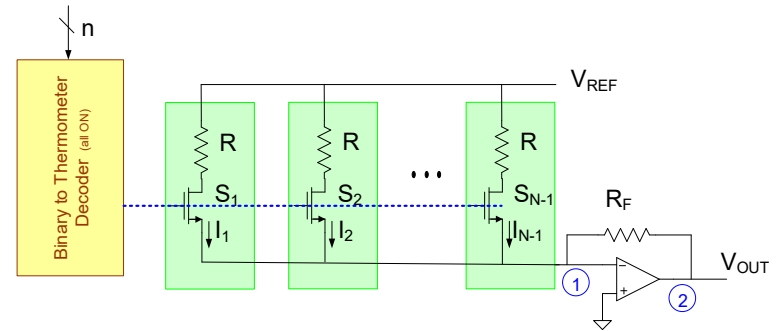
$$\beta = \frac{\frac{R_{CELL}}{k}}{\frac{R_{CELL} + R_F}{k}} = \frac{R_{CELL}}{R_{CELL} + kR_F}$$

If  $V_{OUTFS} = V_{REF}$   $R_{CELL} = NR_F$

$$0.5 < \beta \leq 1$$

# How should the op amp be compensated?

$$\beta = \frac{\frac{R_{\text{CELL}}}{k}}{\frac{R_{\text{CELL}}}{k} + R_{\text{F}}} = \frac{R_{\text{CELL}}}{R_{\text{CELL}} + kR_{\text{F}}}$$

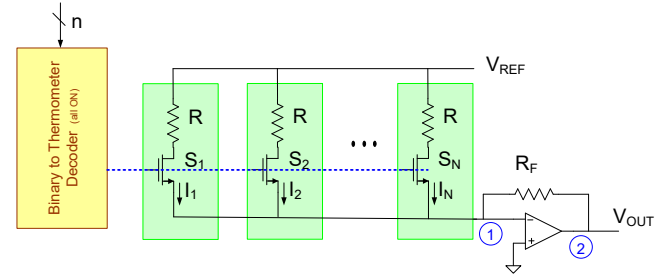
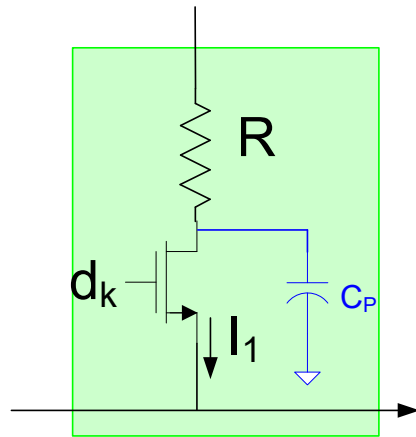


$$V_{\text{OUTFS}} = V_{\text{REF}}$$

$$0.5 < \beta \leq 1$$



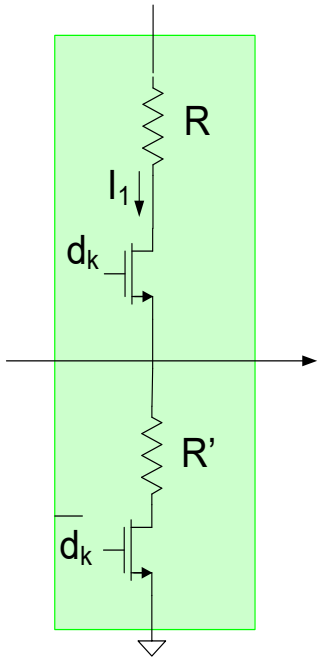
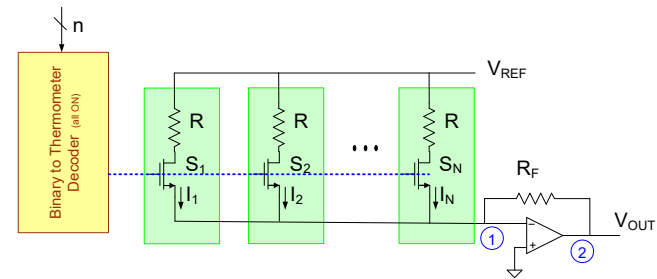
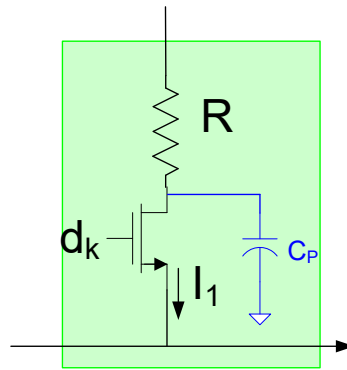
# Current Steering DACs



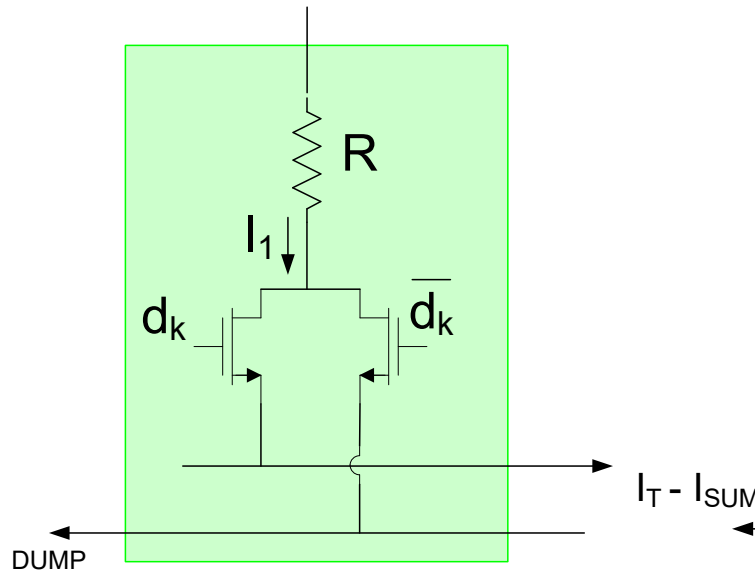
Problem?

Switch impedance	No
Code-dependent phase margin	Yes
Single-ended output	Yes
$C_P$	Yes
Thermometer to Binary Decoder	Yes
Op Amp Bandwidth	Yes
Code-dependent switching time	No

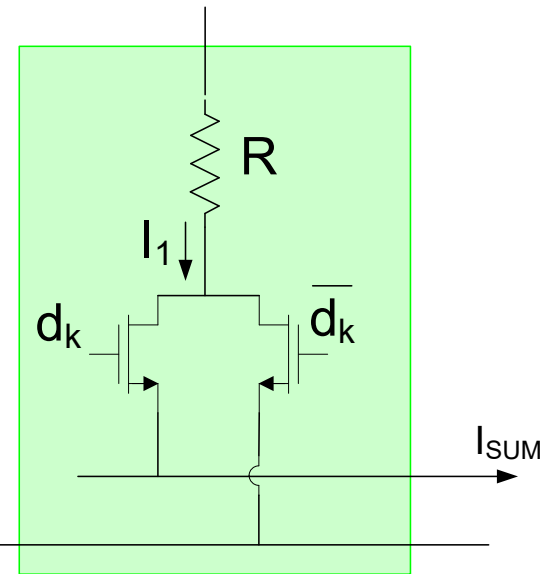
# Current Steering DACs



$\beta$  Compensation



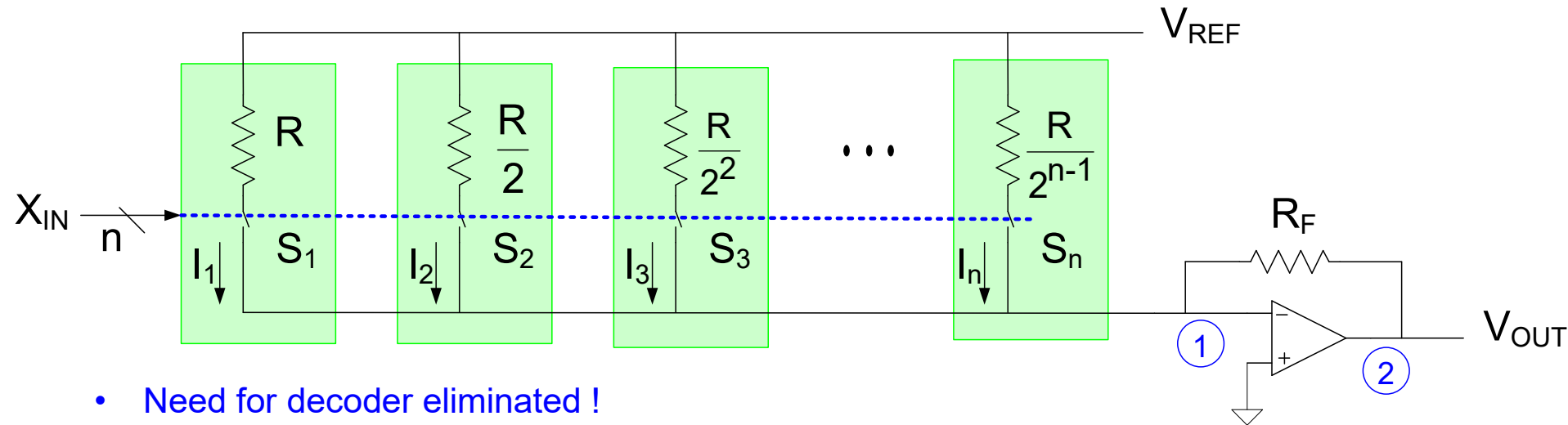
$C_P$  Compensation



Differential Output

# Current Steering DACs

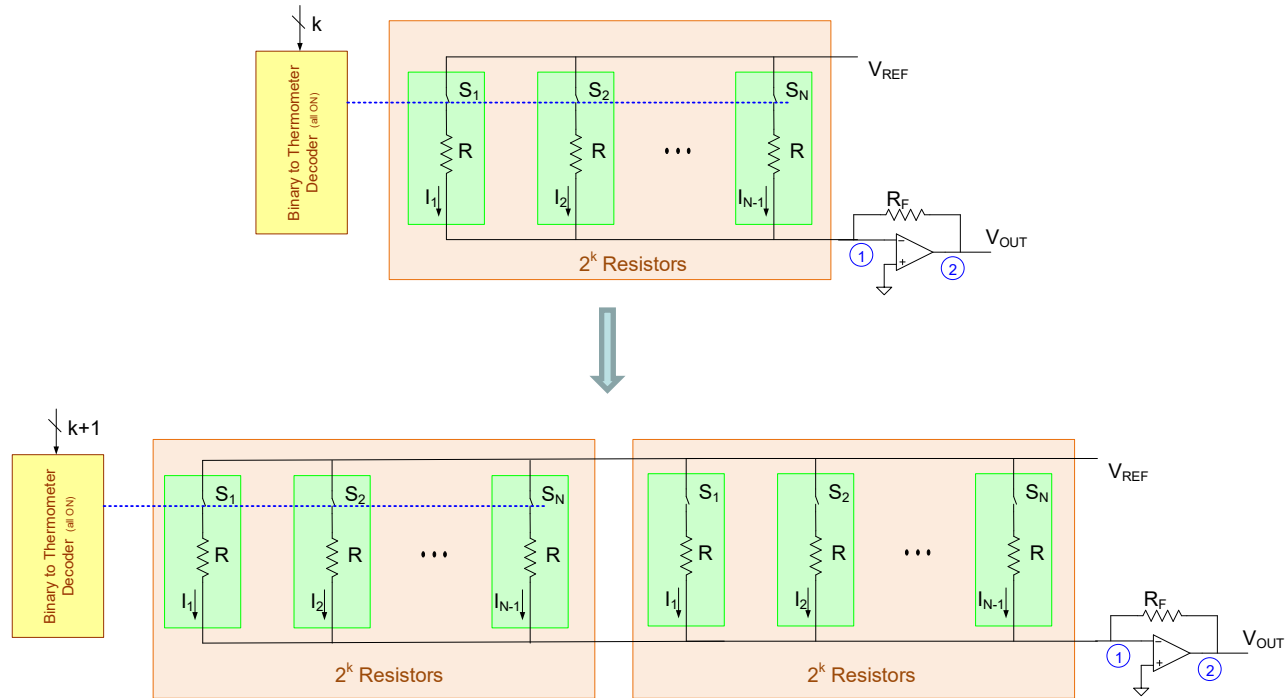
## Binary-Weighted Resistor Arrays



- Need for decoder eliminated !
- DNL may be a major problem
- INL performance about same as thermometer coded if same unit resistors used
- Sizing and layout of switches is critical
- Unary resistor arrays usually used with common-centroid layout(at least for MSB)
- Ratio matching strongly dependent upon area (if common-centroid used to eliminate gradients)
- INL is a random variable with variance approximately proportional to  $\sigma = \frac{A_{PEL}}{\sqrt{A}}$
- Area gets large for good yield with large  $n$

Observe thermometer coding and binary weighted both offer some major advantages and some major limitations

# Current Steering DACs



INL may be poor, typically near mid range

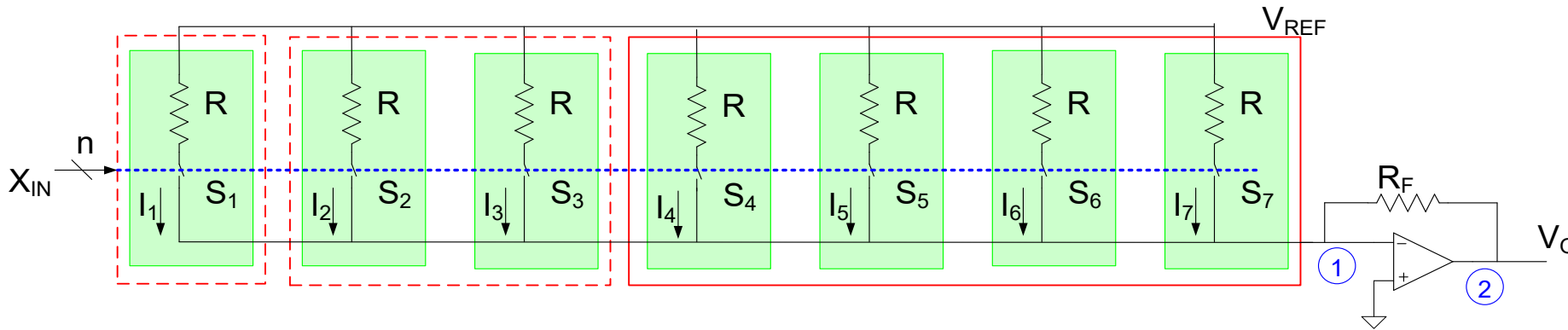
approximately  $\sigma = \frac{A_{PEL}}{\sqrt{A}}$

Consider a k-bit structure that has an acceptable (and desired) yield of Y

Can a k+1 bit structure be easily implemented by simply making 2 copies of the resistor array and adding one bit to the decoder?

The one-afternoon design ?

# Current Steering DACs

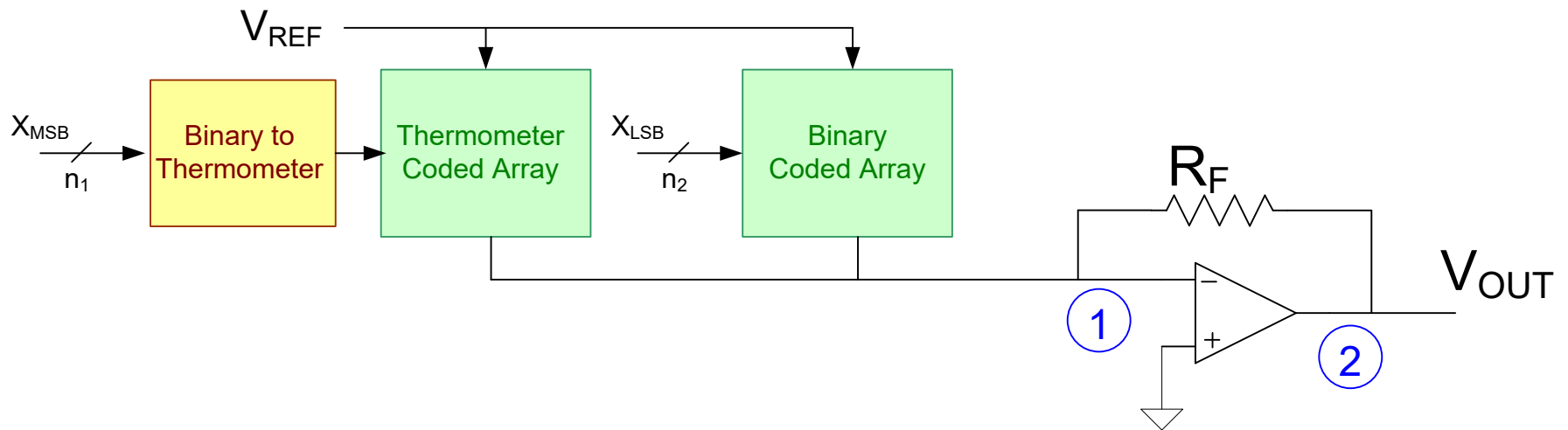


## Binary-Weighted Resistor Arrays

Actual layout of resistors is very important

As stated earlier, bundled unary cells are almost always used

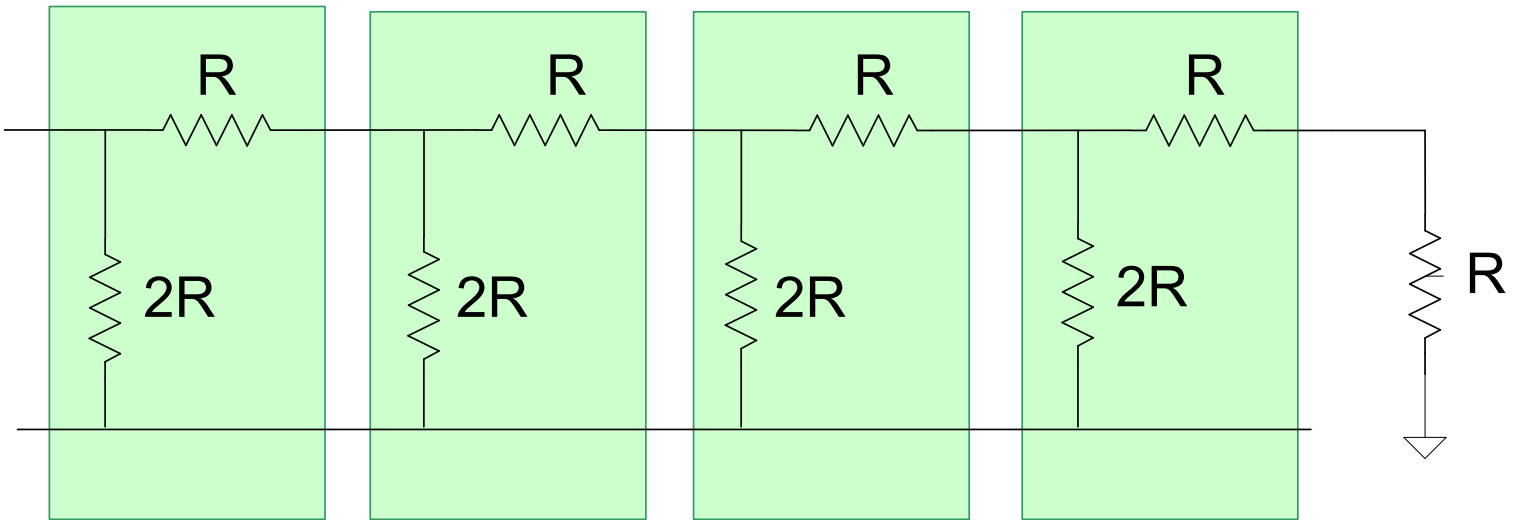
# Current Steering DACs



## Segmented Resistor Arrays

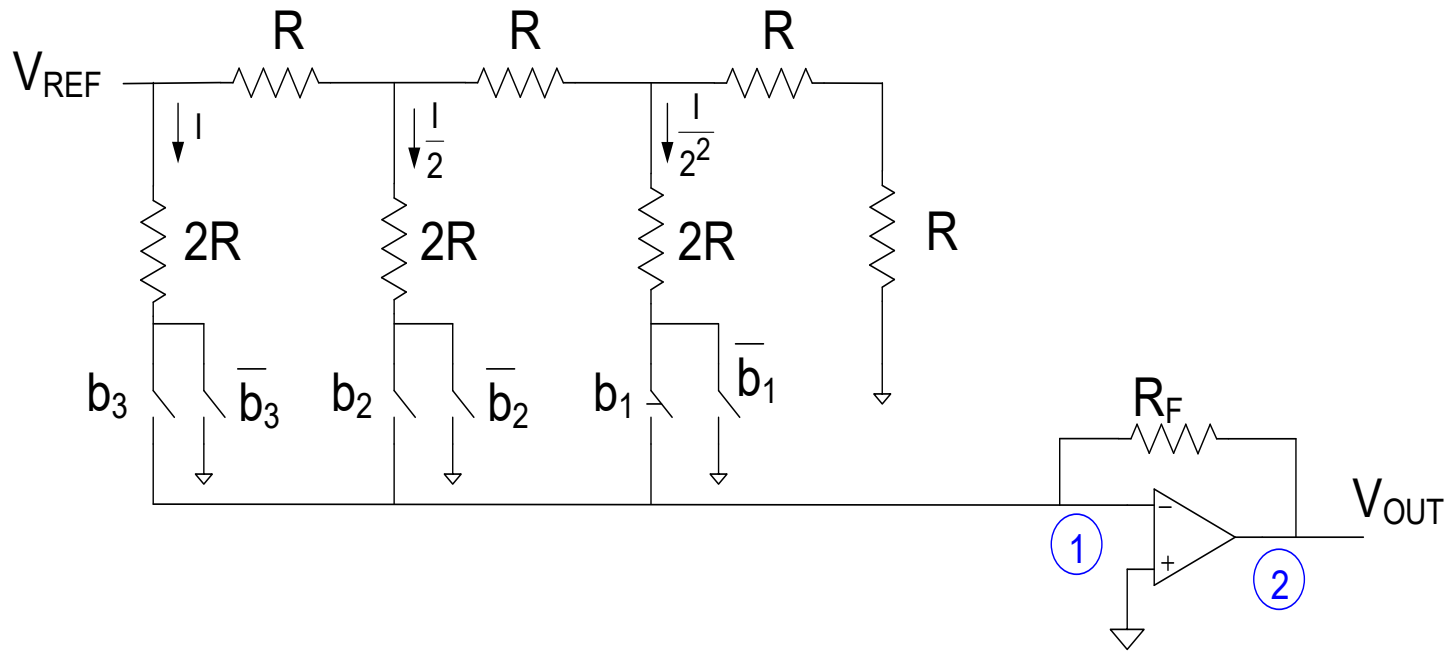
- Combines two types of architectures
- Inherits advantages of both thermometer and binary approach
- Minimizes limitations of both thermometer and binary approach

# R-2R Resistor Arrays



- 4 bit-slices shown
- Can be extended to arbitrary number of bit slices
- Conceptually, area goes up linearly with number of bit slices

# Current Steering DACs



## R-2R Resistor Arrays

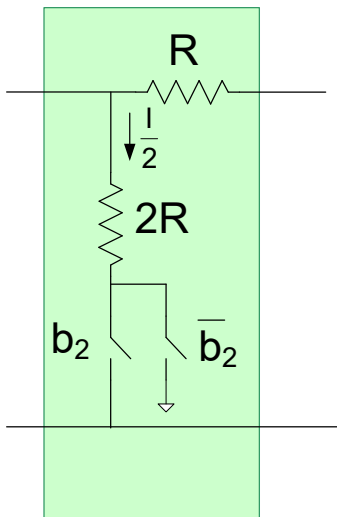
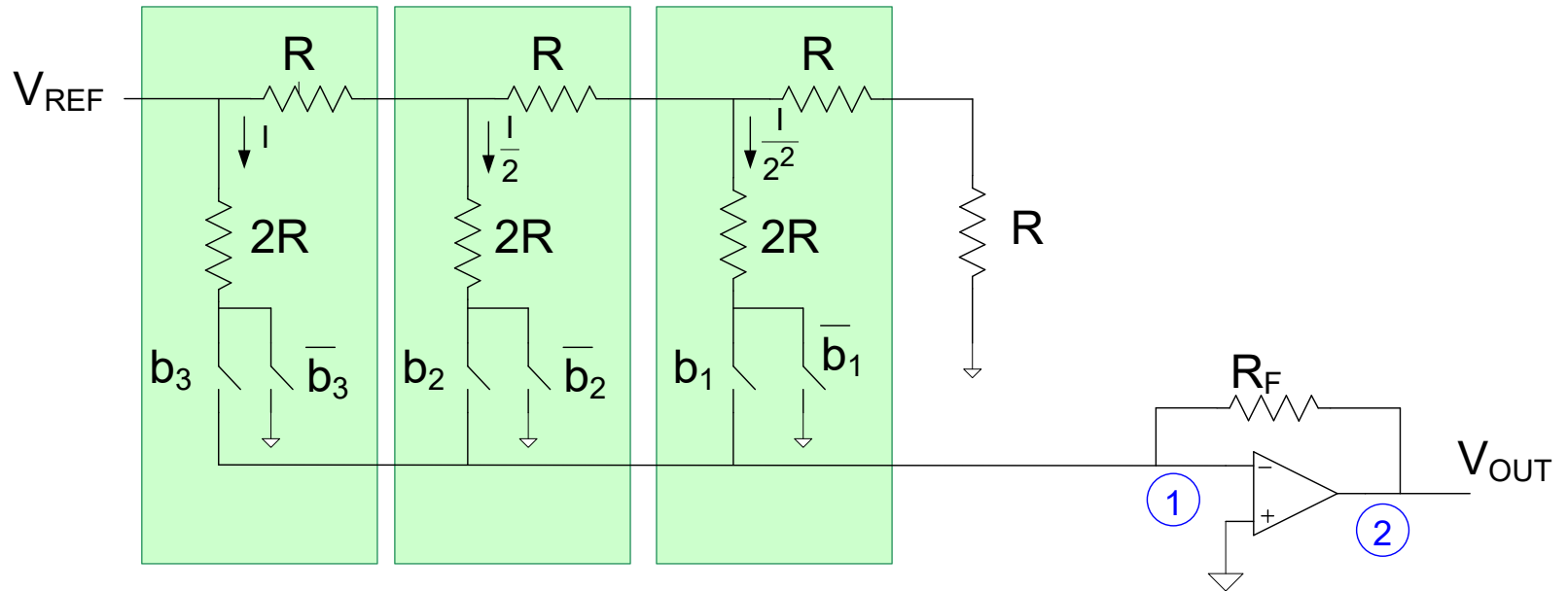
Node voltages ideally stay constant for any input code

Highly sensitive to nonlinearities in switches

How should switches be sized?

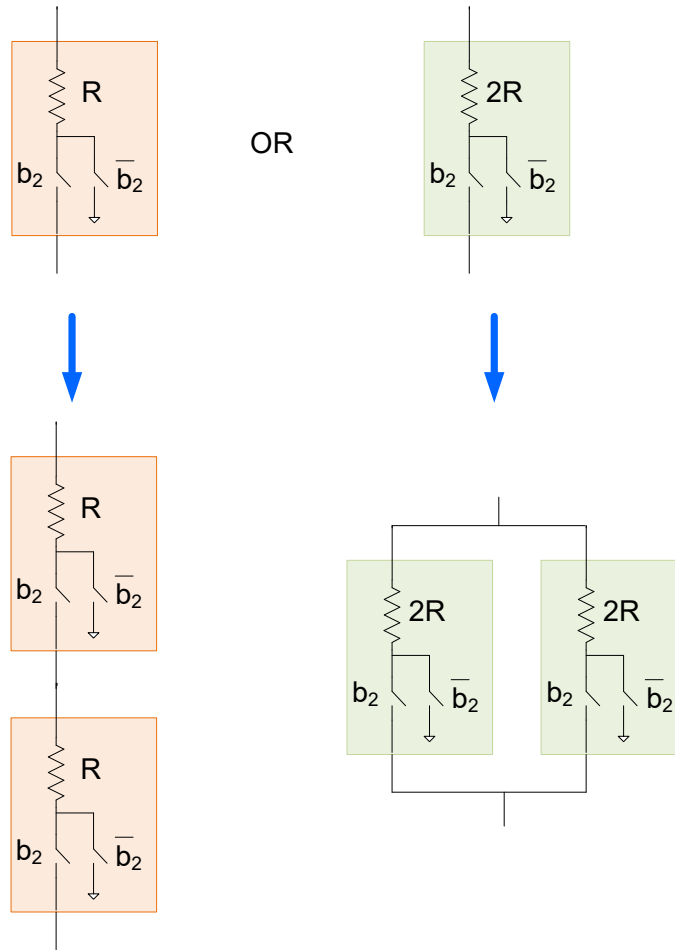


# Current Steering DACs



R-2R Resistor Arrays

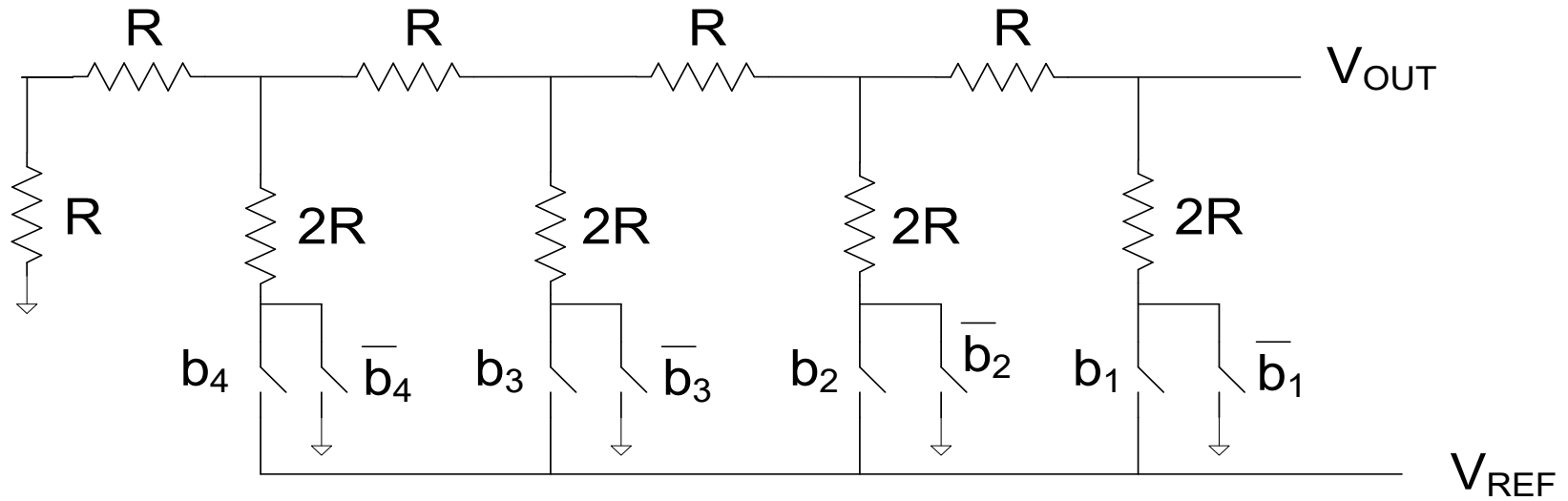
# R-2R Implementation



- Unit cell widely used
- Switch included in cell even if not switched!
- Code dependence of switch impedance of concern

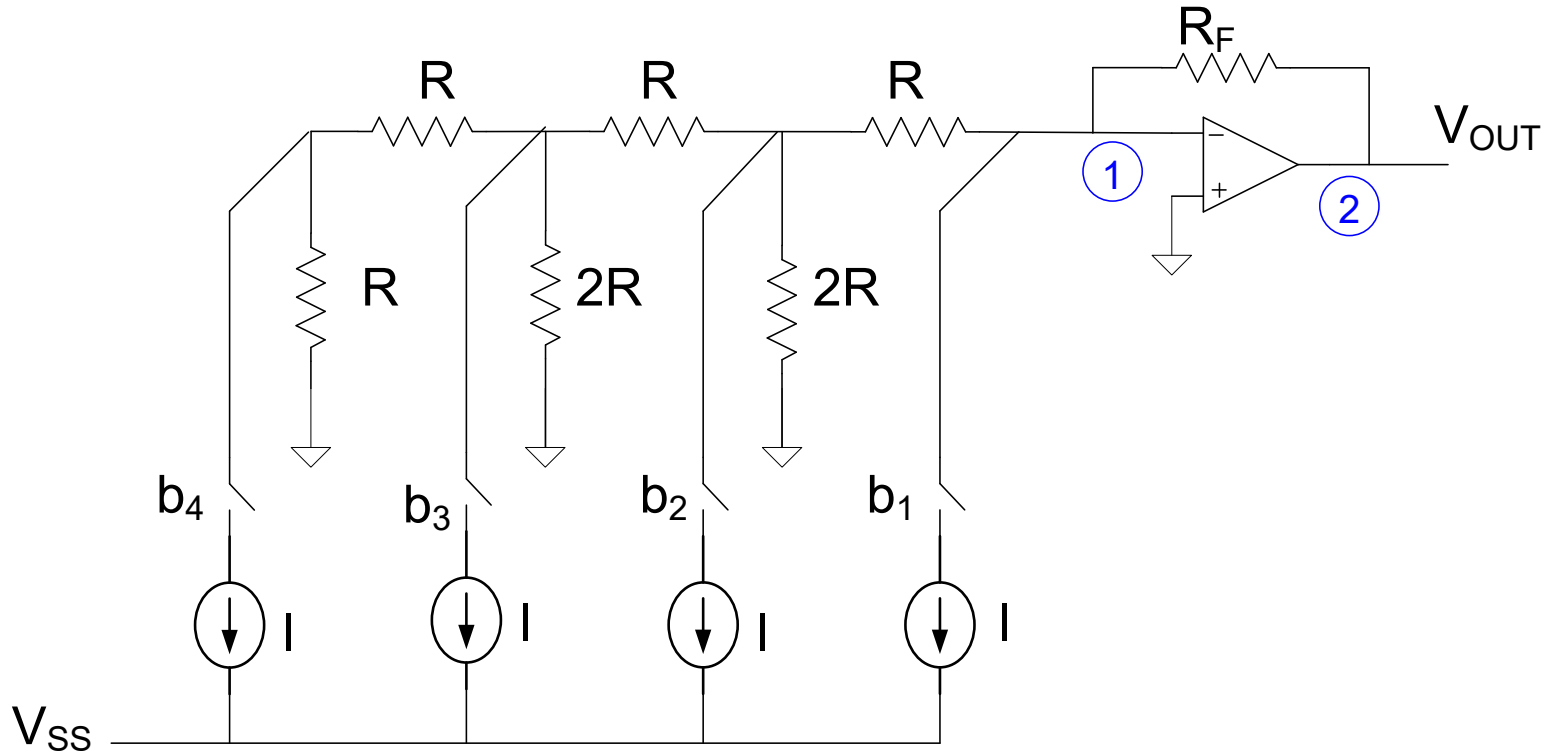
How can switch impedances be matched?

# Another R-2R DAC



Node voltages change with input code

# Another R-2R DAC



Requires matching both current sources and resistors

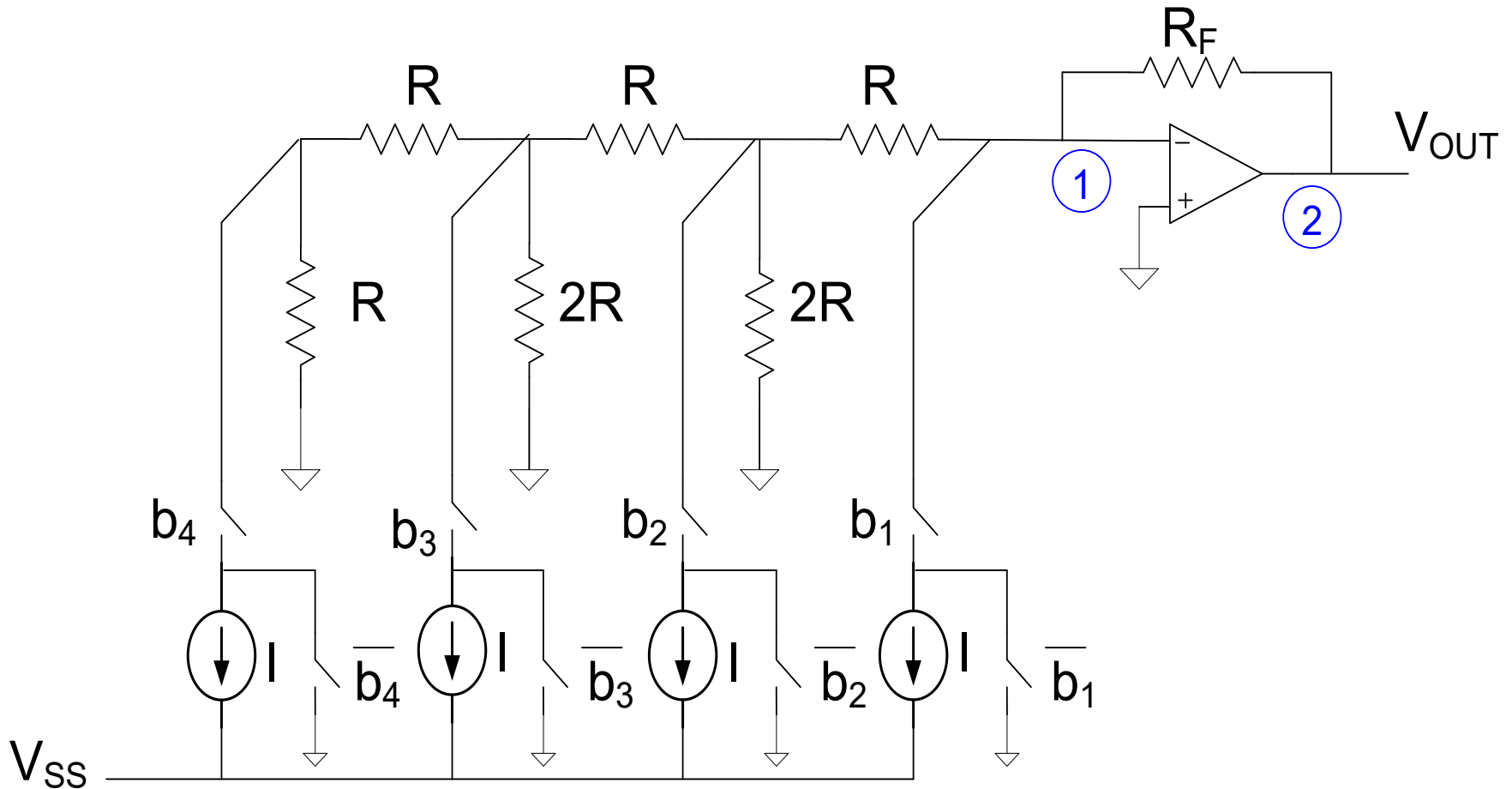
But switch impedance does not affect performance

$\beta$  is independent of Boolean code

Node voltages in R/2R block must change for any input transitions

Voltages on internal R-2R nodes must settle with input transitions

# Another R-2R DAC



Clocks must be nonoverlapping

Does this offer any benefits over previous approach ?

Offers some compensation for capacitances on current sources

Are there other terminations for the current sources?



Stay Safe and Stay Healthy !

End of Lecture 34